

*It is a useful exercise to derive the equations of motion (3.32a-c) from the specification of the Navier-Stokes equations in spherical coordinates  $(r, \vartheta, \varphi)$  such as provided, for example in appendix 2 of Batchelor (2000).*

First consider the isotropic case for which  $A_H = A_V$ .

a. Give an explicit expression for the inertial terms in (3.32a-c).

The expression for the inertial term in (3.32a) is

$$\frac{Du}{dt} - \frac{uv}{r} \tan \theta + \frac{uw}{r} = \frac{\partial u}{\partial t} + \frac{u}{r \cos \theta} \frac{\partial u}{\partial \phi} + \frac{v}{r} \frac{\partial u}{\partial \theta} - \frac{uv}{r} \tan \theta + w \frac{\partial u}{\partial z} + \frac{uw}{r}$$

and the other terms follow similarly.

b. Give an explicit expression for the term  $\mathcal{F}_I^\phi$  in (3.32a-c).

See Batchelor (2000), appendix 2.

Next consider the nonisotropic case, but now in Cartesian coordinates.

c. Give an explicit expression for the term  $\mathcal{F}_I^\phi$  in (3.32a-c) using (3.18).

As we need to compute the divergence of the stress tensor  $\mathcal{T}$ , we use the identity for any vector  $\mathbf{q}$ ,

$$(\nabla \cdot \mathcal{T})\mathbf{q} = \nabla \cdot (\mathcal{T}\mathbf{q})$$

For the component  $\mathcal{F}_I^\phi$  or  $\mathcal{F}_I^x$  in Cartesian coordinates, we can take  $\mathbf{q} = \mathbf{e}_x$ , the unit vector in  $x$ -direction. To compute  $\mathcal{T}(1, 0, 0)^T$  we have to compute

$$\nabla_H \otimes \mathbf{v} + (\nabla_H \otimes \mathbf{v})^T = \begin{pmatrix} 2u_x & v_x + u_y & w_x \\ u_y + v_x & 2v_y & w_y \\ w_x & w_y & 0 \end{pmatrix}.$$

where  $u_x = \partial u / \partial x$ , etc., and

$$\nabla_z \otimes \mathbf{v} + (\nabla_z \otimes \mathbf{v})^T = \begin{pmatrix} 0 & 0 & u_z \\ 0 & 0 & v_z \\ u_z & v_z & 2w_z \end{pmatrix}.$$

It then follows that

$$\mathcal{T} \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} = A_H \begin{pmatrix} 2u_x \\ u_y + v_x \\ w_x \end{pmatrix} + A_V \begin{pmatrix} 0 \\ 0 \\ u_z \end{pmatrix}$$

and hence

$$(\nabla \cdot \mathcal{T}) \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} = A_H(2u_{xx} + v_{xy} + u_{yy} + w_{xz}) + A_V u_{zz}$$

When the flow is incompressible, we can use the continuity equation  $u_x + v_y + w_z = 0$  to get the familiar form

$$(\nabla \cdot \mathcal{T}) \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} = A_H(u_{xx} + u_{yy}) + A_V u_{zz}$$